

**On a Gibbs Measure/Markov Random Field
Representation for Complex Load-Sharing Systems**

by

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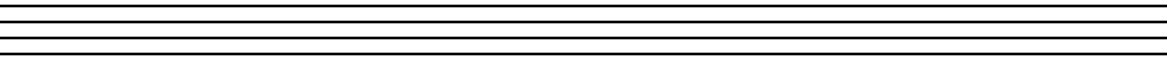
I. Some Objectives of Modeling Complex Systems

- **To model the system**
 - » **Incorporate Component (Marginal/Coupon) Information into the System Model**
 - » **Model Component Dependencies and Interactions**
 - » **Theory Should Be Realistic and Tractable**
 - » **Theory Should Be Composed of Simple Building Blocks**
- **Use “Load-Sharing” to accomplish this**

II. Motivation: Rosen's Experiment

- o Single layer of parallel glass fibers
- o Embedded in an epoxy material (the matrix)
- o Increasing tensile load applied parallel to the fibrous composite until composite fractures
- o Series of pictures identify fiber segment failures
 - Taken at various percentages of the ultimate load.

II. Motivation: Rosen's Pictures

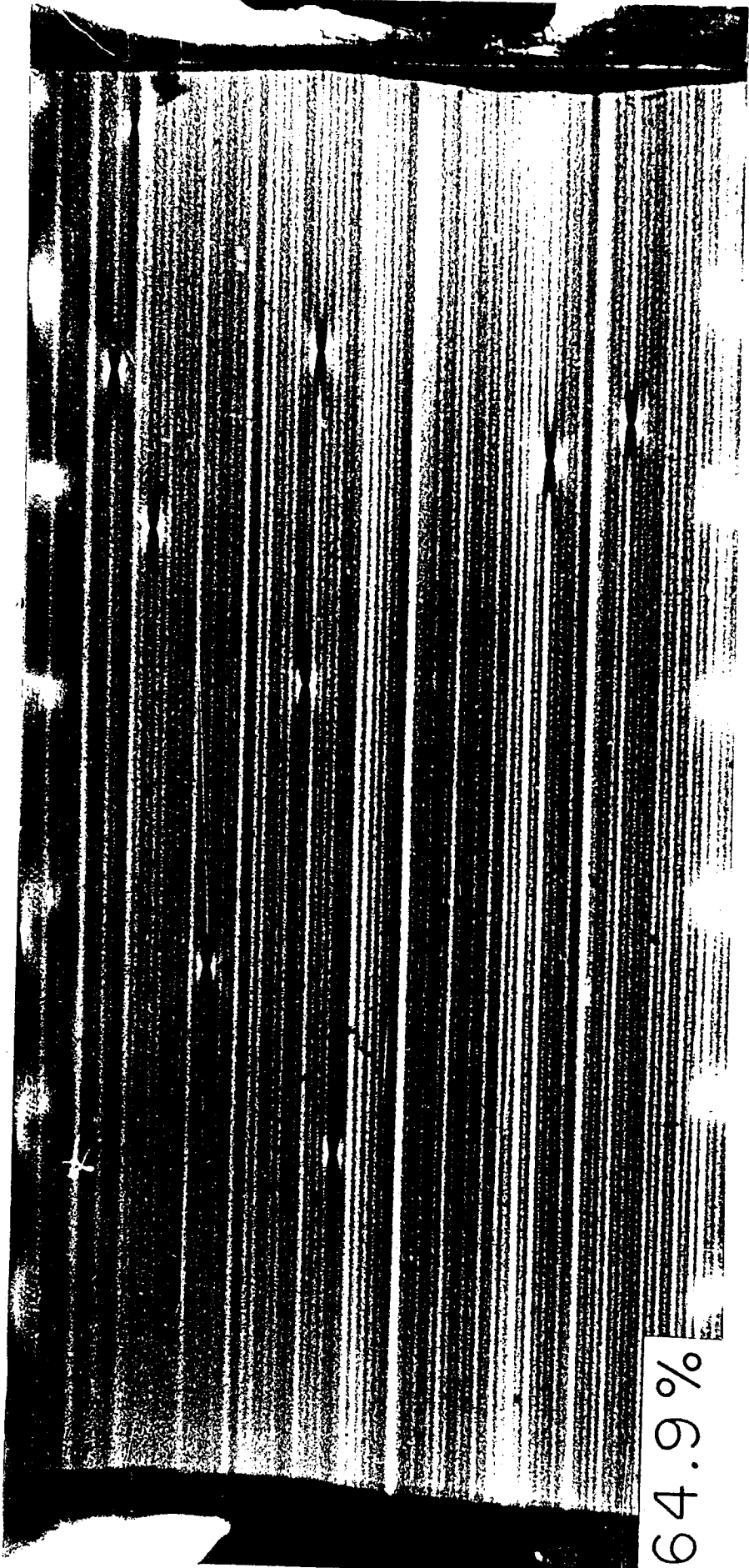


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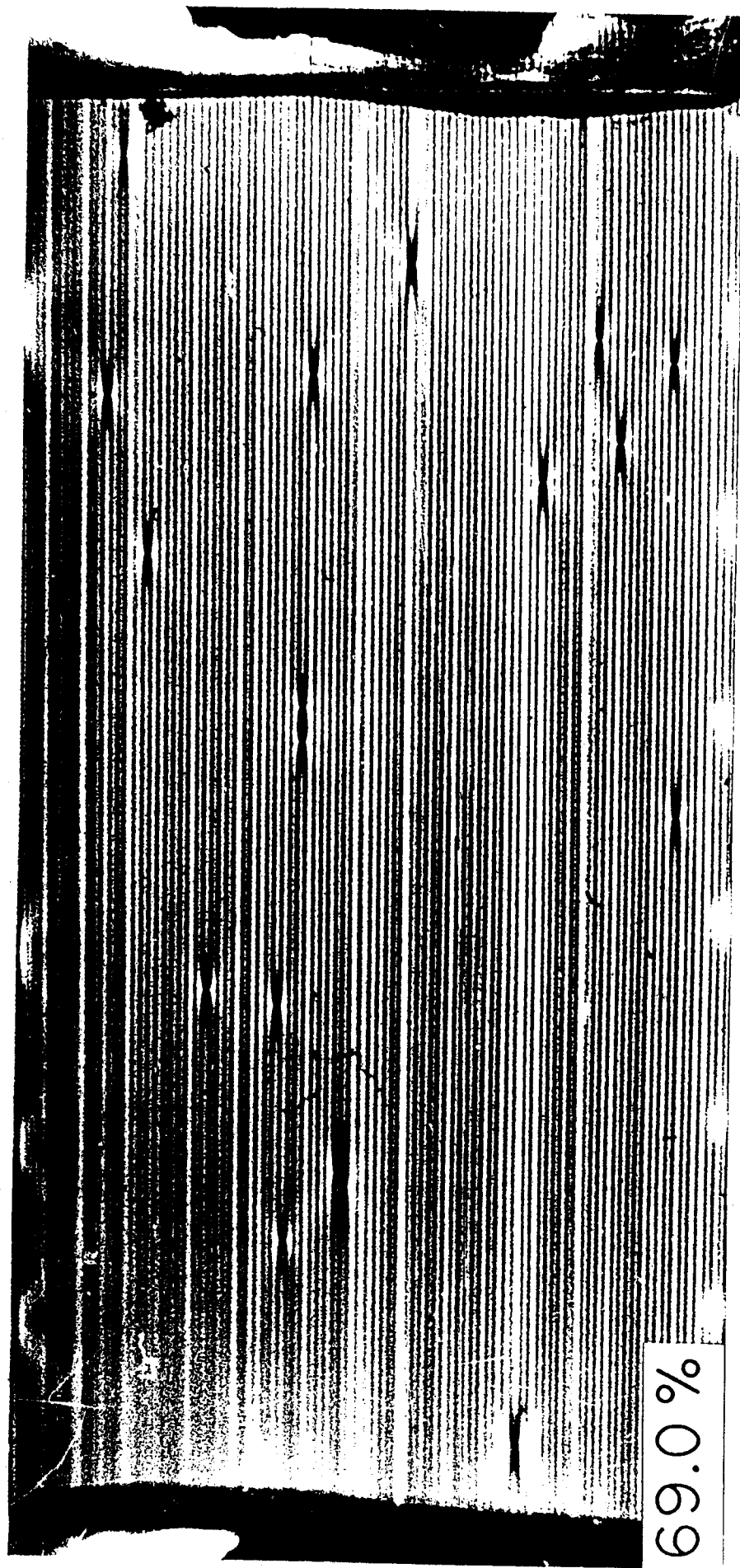
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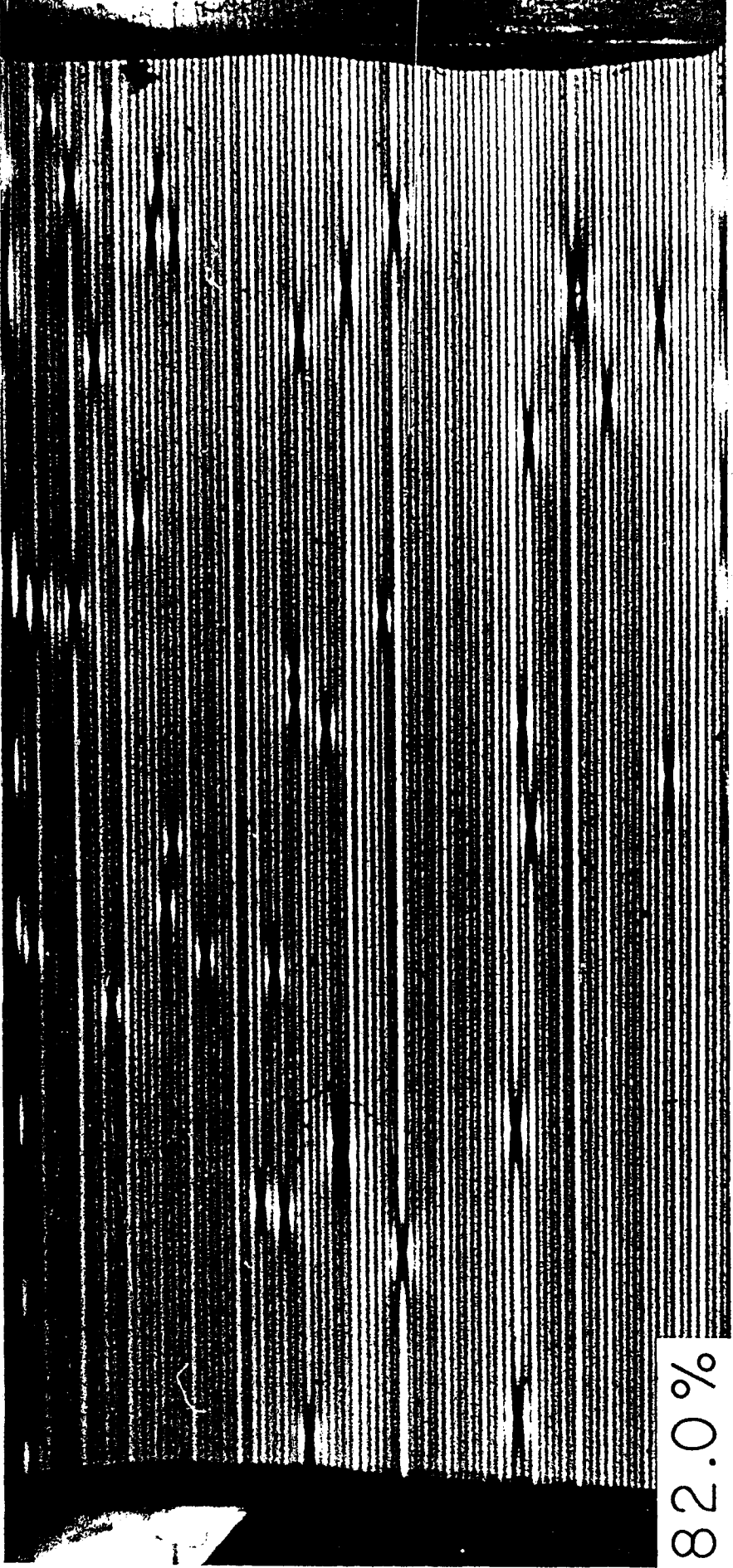
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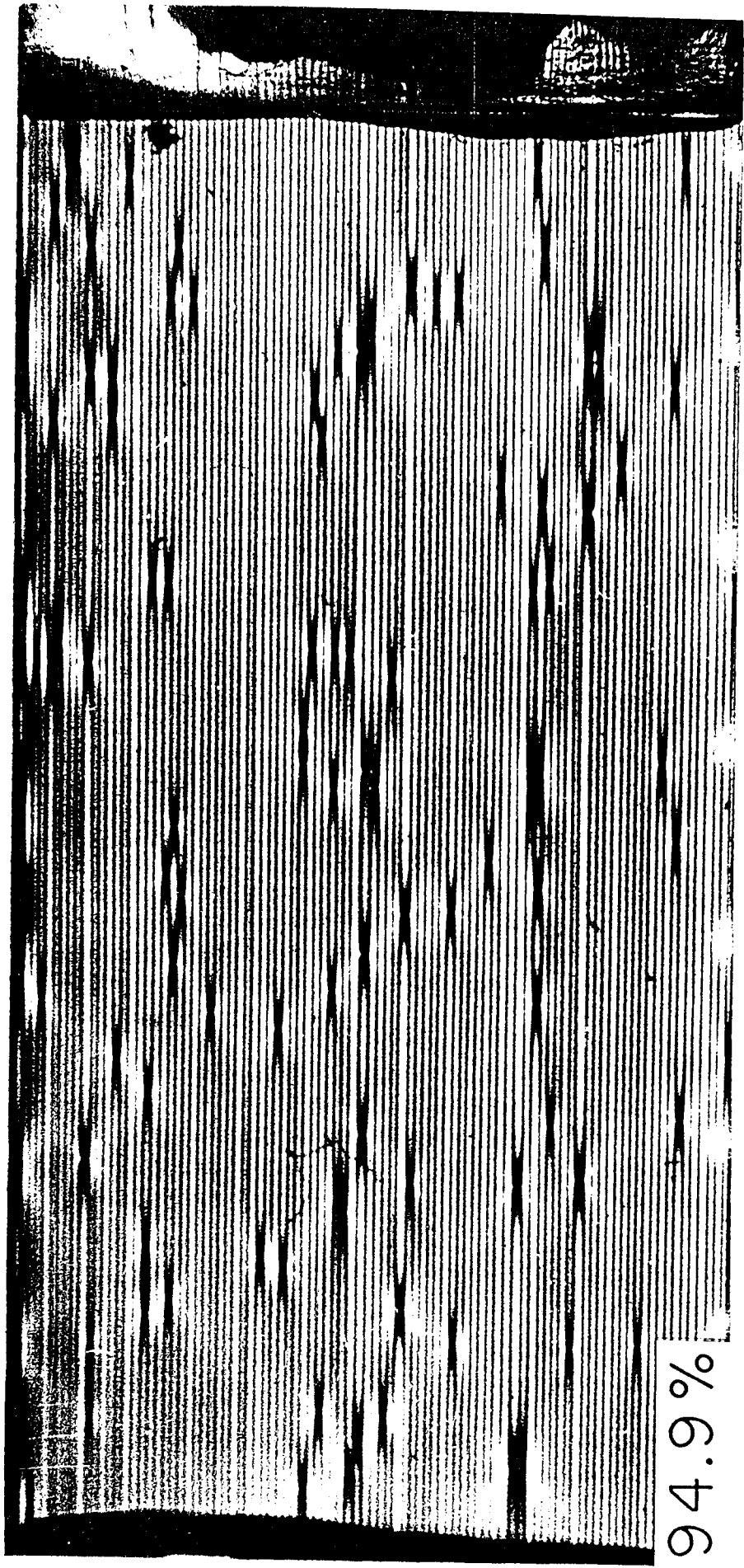
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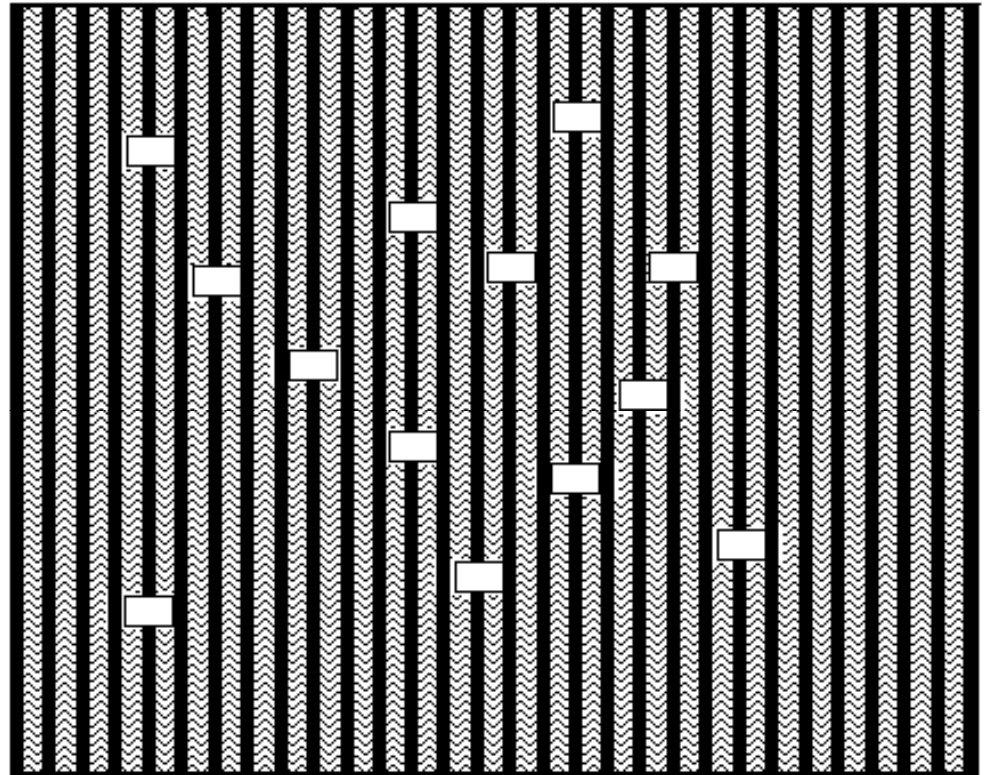


AFTER FAILURE

II. Background

Rosen's Experiment/Ineffective Length

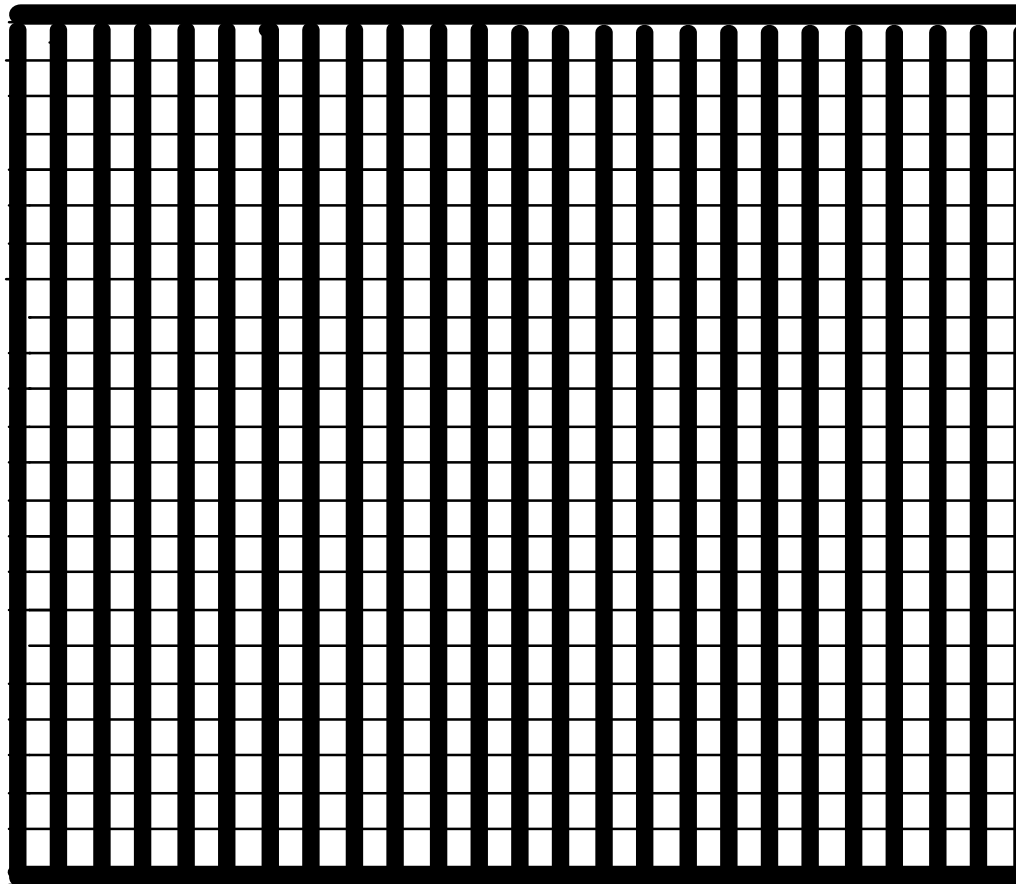
- o Rosen Discovered That There Was No Load Transfer A Certain Distance Around Breaks In Glass Fibers Embedded In A Matrix Material



II. Background: Rosen's Model

An Idealized Model

Ineffective Length



- A System of Independent Components
 - System Is Series-Parallel
 - Series Of Bundles
 - A Bundle Is A Parallel Subsystem
- Dependencies Between Components Are Due To Load Transfer

II. Background

Load Sharing Systems

- **Rosen's Idealized System - Chain of Bundles (Series/Parallel System)**
 - **Bundle was a Parallel System Of Independent Components (Fiber Segments)**
 - **Bundles Independent**
 - **Chain Fails when a Bundle Breaks**
 - **Dependencies Occur Between Components Due To Load Transfer When A Component Fails (Mechanical Consideration)**
 - **Equal Load Sharing in Bundle (Daniels' model)**
- **For Us, System is One (Big) Bundle with Monotone Load Sharing**

III. Load Sharing Rules

Harlow, Smith and Taylor (1983)

o *Load Sharing System*

- n components in a system, $N=\{1,2,\dots,n\}$
- A component load is based on the *nominal load per component* (the load per component or *stress*), say s .
 - » If $M \subseteq N$ denotes the set of working components in N , then the load at component i in M for a nominal load per component s is give by $\lambda_i(M)s$

o *Load Sharing Rule*

- The non-negative constants, $\lambda_i(M)$, define the *load sharing*
- The collection $\{\lambda_i(M) : i \in M, M \subseteq N\}$ is called a *load sharing rule*

III. Montone Load Sharing Rules

System Strength

- o A load sharing rule is referred to as a *monotone load sharing rule* if

- $\lambda_i(L) \geq \lambda_i(M)$ for all $i \in L, L \subseteq M \subseteq N,$

- $\sum_{i \in M} \lambda_i(M) > 0$ for all $M \subseteq N.$

- o *System Strength* is given by where X_i is the strength of the i^{th} component. P^* is set of path sets for system

$$S = \max_{M \in P^*} \min_{i \in M} \frac{X_i}{\lambda_i(M)}$$

IV. Evolution of Component Failures

Phase I/II cycles of failures

- Under increasing load the system incurs component failures as follows:
 - The system incurs a series of K Phase I failures due to load sharing at nominal loads per components $S_1 < S_2 < \dots < S_K = S$
 - The set of working components just prior to breaking stress S_i is A_i . Note that $A_1 = N$. Let $X_{\underline{u}(i)}$ denote the component strength of the component that fails at S_i . Then $X_{U(i)} = \lambda_{U(i)}(A_i)S_i$.
 - When component $U(i)$ fails, sudden load transfer causes a series of component failures (Phase II failures). The set of working components after these failures is A_{i+1} .

IV. Evolution of Component Failures

Phase I/II cycles of failures – Markovian Structure

- Under monotone load sharing and independent components

- $S_m \mid S_i \ i \leq m-1, A_i \ i \leq m =_d S_m \mid S_{m-1}, A_m$

$$(S_m = \min_{i \in A_m} \frac{X_i}{\lambda_i(A_m)} > S_{m-1})$$

- $U(m) \mid S_i \ i \leq m, A_i \ i \leq m, U(i) \ i \leq m-1 =_d U(m) \mid S_m, A_m$
 - $A_{m+1} \mid S_i, A_i \ i \leq m, U(m) =_d A_{m+1} \mid S_m, A_m, U(m)$

and is a Markov Random Field on A_m with Gibbs measure

$$P_{S_m, A_m, U(m)}(A), A \subseteq A_m - U(m)$$

- $\{(A_1, S_1, U(1)), \{(A_2, S_2, U(2)), \dots\}$ is a Markov chain.

IV. Evolution of Component Failures

Phase I/II cycles of failures – Markovian Structure

1.
$$S_m = \min_{i \in A_m} \frac{X_i}{\lambda_i(A_m)} \rightarrow U(m) \rightarrow A_{m+1} \subseteq A_m - \{U(m)\}$$

$$A_{m+1} \rightarrow S_{m+1} \rightarrow U(m+1) \rightarrow A_{m+2} \rightarrow \dots$$

2. $U(m)$'s distribution is determined by the failure rates at S_m of the components in A_m

3. $P_{S_m, A_m, U(m)}(A)$, $A \subseteq A_m - \{U(m)\}$ is the GM

V. GM/MRF Representation

Preliminaries

- o **Finite Undirected Graph $G=(N,E)$**
 - $N=\{1,2,\dots,n\}$ set of n nodes, E =set of edges
 - Edges determine neighbors, δ_i denotes the neighbors of node i
 - Cliques are sets of nodes all of which are neighbors of one another
- o **MRF on G**
 - Y_1, \dots, Y_n node rv's taking values in some finite set S
 - For $\omega_k \in S$, $P(Y_i = \omega_i | Y_j = \omega_j, j \in N - \{i\}) = P(Y_i = \omega_i | Y_j = \omega_j, j \in \delta_i)$
- o **GM on G**
 - Potentials: $V_A(\underline{\omega})$, $\underline{\omega} \in S$, A a subset of N
 - Energy: $U(\underline{\omega}) = - \sum_{A \subseteq N} V_A(\underline{\omega})$
 - Partition function: $Z = \sum_{\underline{\omega} \in S^n} \exp\{-U(\underline{\omega})\}$
 - GM: $P(\underline{Y} = \underline{\omega}) \equiv P(\underline{\omega}) = \frac{\exp\{-U(\underline{\omega})\}}{Z}$

V. GM/MRF Representation

Preliminaries

- o **Canonical Energy and Potentials:**

$$\tilde{U}(\underline{\omega}) \equiv U(\underline{\omega}) - U(\underline{0}) \quad \text{and} \quad \tilde{V}_A(\underline{\omega}) \equiv \sum_{B \subseteq A} -1^{|A-B|} \tilde{U}(\underline{\omega}^B)$$

- o **Nearest Neighbor Potentials:**

$$\tilde{V}_A(\underline{\omega}) \text{ is a NN potential and } \tilde{U}(\underline{\omega}) = - \sum_{A \subseteq N} \tilde{V}_A(\underline{\omega})$$

1. NN Potential means \tilde{V}_A vanishes if A is not a clique

2. $\tilde{V}_A(\underline{\omega}) = 0$ if $\omega_i = 0$ for some $i \in A$.

V. GM/MRF Representation for *LS* system

Static Case

- o MRF on directed graph $G^*=(N,E^*)$

- Y_1, \dots, Y_n node rv's taking values in $S=\{0,1\}$
- Let I_i be the set of indices in the smallest collection of rv's such that

$$P(Y_i = 1 | Y_j = \omega_j, j \in N - \{i\}) = P(Y_i = 1 | Y_j = \omega_j, j \in I_i)$$

- Definitions:

* j influences i ($j \rightarrow i$) if $j \in I_i$.

* Sites i and j are called neighbors if either $j \rightarrow i$ or $i \rightarrow j$.

* The set $N_i = \{j: j \rightarrow i \text{ or } i \rightarrow j\}$.

- Consequences: Since N_j contains I_j ,

$$P(Y_i = 1 | Y_j = \omega_j, j \in N - \{i\}) = P(Y_i = 1 | Y_j = \omega_j, j \in N_j) = P(Y_i = 1 | Y_j = \omega_j, j \in I_j)$$

V. GM/MRF Representation for *LS* system

Static Case: Local Structure of MRF

- o **Log odds ratio for node i :**

$$\sigma_i(A, s) \equiv \frac{P(Y_i = 1 | Y_j = 1, j \in A - \{i\}, Y_k = 0, k \in A^c)}{P(Y_i = 0 | Y_j = 1, j \in A - \{i\}, Y_k = 0, k \in A^c)} \quad (A)$$

$$= \frac{P(Y_i = 1, Y_j = 1, j \in A - \{i\}, Y_k = 0, k \in A^c)}{P(Y_i = 0, Y_j = 1, j \in A - \{i\}, Y_k = 0, k \in A^c)} \quad (B)$$

- o **Let F_i denote the strength distribution of component i and $S_i = 1 - F_i$ the strength survival distribution. From (A),**

$$\sigma_i(A, s) = \ln \frac{S_i(\lambda_i(A)s)}{F_i(\lambda_i(A)s)} \quad (C)$$

while from (B) and the canonical potential representation for GM's

$$\sigma_i(A, s) = \sum_{\{K \subseteq A, i \in K\}} V_K(\underline{\omega}(A), s) \quad (D)$$

where $\underline{\omega}(A)$ is the vector of component states with

$\omega_i = 1$ if $i \in A$ and $= 0$ if $i \notin A$.

V. GM/MRF Representation for LS system

Log Odds is the Primitive

o Consequences of (A)-(D)

- (A) and (C) imply that the LS-Rule determines G^*
- (C) and (D) with the Mobius inversion formula give

$$V_K(\underline{\omega}(K), s) = \frac{\sum_{A \subseteq K} \sum_{i \in A} (-1)^{|K-A|} \sigma_i(A, s)}{|K|}$$

- In the dynamic case, replace the component strength distributions by conditional ones, conditional on $X_i > \lambda_i(A_m) S_m$

Concluding Comments

- Simple formulas if the component strength distributions are log-logistic. Useful in understanding the system structure.
- Static case does not depend on monotone LS to get the GM/MRF
- Conjecture that above rep works for arbitrary LS. Just get recursive formulas for the conditional distributions that depend on the whole history.
- Can generate an “exact” sample of system failure which can involve lots of comparisons of component strengths depending on the asymmetry and spatial dependence of the LS rule.
- Doubly Intractable Issues (Iain Murray talk at Duke in January 2009)

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